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## Emission characteristics of coal combustion in different $O_2/N_2$ , $O_2/CO_2$ and $O_2/RFG$ atmosphere

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#### Abstract

This study investigates the emission characteristics of  $CO_2$ ,  $SO_2$  and NOx in the flue gas of coal combustion by varying the compositions and concentrations of feed gas  $(O_2/CO_2/N_2)$  and the ratios of recycled flue gas. The differences between  $O_2$ /recycled flue gas  $(O_2/RFG)$  combustion and general air combustion are also discussed. Experimental results indicate that the maximum concentration of  $CO_2$  in  $O_2/CO_2$  combustion system is 95% as the feed gas is 30%  $O_2/70\%$   $CO_2$ . The average concentration of  $CO_2$  in the flue gas of  $O_2/CO_2$  coal combustion system is higher than 90% and much higher than that of  $O_2/N_2$  coal combustion system. This high concentration of  $CO_2$  is beneficial for the separation of  $CO_2$  from the flue gas by adsorption or absorption technologies. The maximum concentration of  $CO_2$  in  $O_2/N_2$  combustion system is only 34% at the feed gas 50%  $O_2/50\%$   $N_2$ , the concentration of  $CO_2$  is increased with the concentration of  $O_2$  in feed gas.

By  $O_2/CO_2$  combustion technology, higher concentration of  $SO_2$  is produced as the feed gas is 30%  $O_2/70\%$   $CO_2$  or 40%  $O_2/60\%$   $CO_2$ , while higher concentration of NOx is produced as the feed gas is 20%  $O_2/80\%$   $CO_2$  or 50%  $O_2/50\%$   $CO_2$ . The mass flow rates of  $CO_2$ ,  $CO_2$  and NOx in the flue gas are all increased with the ratio of recycled flue gas except for the feed gas 20%  $CO_2/80\%$   $CO_2$ . The enhanced mass flow rates of air pollutants in such  $CO_2/RFG$  combustion system are also beneficial for improving the control efficiencies of air pollution control devices. By  $CO_2/NO_2$  combustion technology, higher concentrations of  $CO_2/RFG$  and  $CO_2/RFG$  or  $CO_2/CO_2/RFG$  or  $CO_2/CO_2/RFG$  or  $CO_2/CO_2/CO_2/CO_2$  combustion system.

Keywords: Coal combustion; O2/CO2; O2/RFG; SO2; NOx

### 1. Introduction

As the global warming and climate change due to greenhouse effects are continuing serious, mitigating the emission of greenhouse gas  $CO_2$  becomes an international and imperative issue. Since only 21% oxygen is contained in the auxiliary air, the concentration of  $CO_2$  formed in general air combustion system is usually lower than 15%. The other 79% nitrogen in the auxiliary air is released as exhaust gas and consumes a lot of heat energy. The low concentration of  $CO_2$  in the exhaust gas is the major reason that leads the removal efficiency of  $CO_2$  by general end-of-pipe separation technologies ineffective. The major strategies for  $CO_2$  control include physical adsorption, under-

ground or seabed storage, chemical absorption, and organism fixation, etc. [1-3]; and the technologies for separating  $CO_2$ from exhaust gas include physical adsorption, physical absorption, chemical absorption, cryogenic distillation, and membrane separation [4–8]. Practically, the removal efficiency of CO<sub>2</sub> by these technologies is usually depressed due to the deteriorations and poisons of sorbents in the presences of other air pollutants such as NOx, SOx, HCl, fly ash, and O2. For improving the removal efficiency of CO<sub>2</sub>, a lot of extra energy has been consumed [9]. Therefore, many researchers are devoted to develop the "Clean Coal Combustion Technology" or "Clean Combustion Technology". O<sub>2</sub>/RFG or O<sub>2</sub>/CO<sub>2</sub> combustion technology is one of the clean combustion technologies, and has been studied and applied at coal-fired power plants in Japan and Europe. Moreover, some novel coal combustion technologies such as MATIANT cycle and ZEPP (near zero emission power plants) derived from  $O_2/RFG$  or  $O_2/CO_2$  are also developed [10–12].

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O<sub>2</sub>/RFG combustion technology is originated in 1992. The technology separates the nitrogen from air and the remained pure oxygen is mixed with the recycled flue gas (the major gas is CO<sub>2</sub>) to serve as the feed gas. The concentration of CO<sub>2</sub> in exhaust gas could be significantly increased and the recovery of CO<sub>2</sub> becomes feasible. As reported in the references, the concentration of CO2 in the flue gas can be increased to higher than 95% by such O<sub>2</sub>/RFG combustion technology. This high concentration of CO<sub>2</sub> is beneficial for the recovery and control [13]. The CO<sub>2</sub> recycled coal-combustion system and the CO<sub>2</sub> recycled IGCC (integrated gasification combined cycle) system which also apply this O<sub>2</sub>/RFG combustion technology are demonstrated to be the most economic and effective combustion system for power generation [14]. Yamada et al. [15] addressed that the conversion of NOx in air combustion was 30% higher than that in O<sub>2</sub>/CO<sub>2</sub> combustion. The emission of NOx and SO<sub>2</sub> could be reduced in O<sub>2</sub>/CO<sub>2</sub> combustion. Croiset and Thambimuthu [16] also indicated that the emission of NOx in different combustion atmospheres followed the sequence of air  $> O_2/CO_2$  without recycled flue gas  $> O_2/CO_2$  with recycled flue gas, and the emission of SO<sub>2</sub> also followed the sequence of air  $> O_2/CO_2$  without recycled flue gas  $> O_2/CO_2$  with recycled

Since the  $O_2/RFG$  combustion technology is still in development and many researches focus on its application in power plant and  $CO_2$  recovery, the emission characteristics of other pollutants such as NOx and  $SO_2$  are seldom investigated. The relative studies are never present in Taiwan. Therefore, this study completely investigates the emission characteristics of  $CO_2$ , NOx and  $SO_2$  at different combustion atmospheres. The effects of different operating conditions are also discussed. These results will provide useful references for the applications of  $O_2/RFG$  combustion technology in the future.

### 2. Experimental

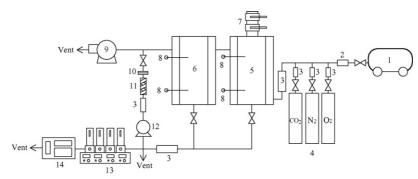
### 2.1. Experimental apparatus

Fig. 1 shows the schematic diagram of experimental apparatus. The feed gas with different gas composition and concen-

trations was prepared by using gas cylinders, air compressor, mass flow meters and gas mixer. For a better control of combustion temperature, a fluidized bed incinerator was used as the experimental reactor. The fluidized bed incinerator is consisted of a feedstock feeder, a main combustion chamber and a secondary combustion chamber of 50 cm height and 5 cm inside diameter. All the chambers are made of 3 mm thick stainless steel (AISI 310). Five thermocouples were inserted into the axis to determine the temperatures in first and secondary combustion chambers and flue gas pipe. Silica sand was used as bed material and its particle size distribution was 300 µm 49.62%,  $214 \mu m$  17.35%, 470  $\mu m$  15.05%, and <163  $\mu m$  12%. Because fluidized bed incinerator has better heat capacity and mixing efficiency, the temperature distribution in the combustion chamber is uniform and stable. The average deviation of incineration temperature in our experiments was controlled within 20 °C. The granular coal was fed into the incinerator by a rotary feeder on the top of fluidized bed incinerator. The exhaust gas was treated by a baghouse, a wet scrubber and finally discharged into the atmosphere. The granular coal used in this work was the bituminous coal produced from Indonesia and it was also used at one coal-fired power plant in Taiwan. The chemical compositions of the coal are 65.53% C, 4.78% H, 13.24% O, 2.6% N and 1.12% S. The coal was pretreated by drying, grinding, and screening. The heating value of dry coal is  $6145 \text{ cal g}^{-1}$  and the particle size of coal was controlled in the range of 833–1651 μm.

#### 2.2. Experimental procedures

Before performing the experiment, the first and secondary combustion chambers were preheated by electric heaters to 800 and 1000 °C, respectively. The prepared feed gas with desired gas composition and concentration was introduced into the combustion system to verify the airtight of pipeline and the concentration of feed gas. After the temperature in combustion chambers reached steady state, the experiment started and the granular coal was continuously fed into the incinerator at a feed rate of 4 g min<sup>-1</sup>. The flow rate of feed gas in each run was controlled at 20 L min<sup>-1</sup>. The detailed operating conditions for each run are listed in Table 1.



- 1. Air compressor 2. Dehumidifer 3. Gas flow meter 4. Feed gas cylinder
- 5. First combustion chamber 6. Second combustion chamber 7. coal feeder
- 8. Thermocouple 9. Induced fan 10. Fly ash filter 11. Vapor condenser
- 12. Sampling pump 13. Dilution system 14. Flue gas analyzer

Fig. 1. Schematic diagram of experimental apparatus.

Table 1 Experimental conditions

Run	Feed gas composition (vol.%)			Recycled flue gas (vol.%)
	$\overline{\mathrm{O}_2}$	CO <sub>2</sub>	N <sub>2</sub>	
1–5	20	80	_	0, 30, 40, 50, 60 (1) <sup>a</sup>
6-14	30	70	_	$0, 30, 40, 50, 60 (1, 2)^a$
15-23	40	60	_	$0, 30, 40, 50, 60 (1, 2)^a$
24-28	50	50	_	$0, 30, 40, 50, 60 (1)^a$
29-33	21	_	79	$0, 30, 40, 50, 60 (1)^a$
34-42	30	_	70	$0, 30, 40, 50, 60 (1, 2)^a$
42-51	40	_	60	$0, 30, 40, 50, 60 (1, 2)^a$
52-56	50	_	50	0, 30, 40, 50, 60 (1) <sup>a</sup>

<sup>&</sup>lt;sup>a</sup> 1: recycling flue gas to first combustion chamber; 2: recycling flue gas to second combustion chamber

The temperature profiles of combustion chambers and the concentrations of  $CO_2$ , NOx and  $SO_2$  in the exhaust gas were monitored and recorded during the experiment according to the standard analysis procedures [17–19]. The coal feed rate and feed gas flow rate were checked and controlled for stability during the experiment. The flue gas was passed through a glass-fiber filter to remove fly ash, dewatered by a vapor condenser, and then analyzed by a flue gas analyzer (HORIBA, PG-250). This flue gas analyzer uses non-dispersive IR detection for CO and  $CO_2$ , and a galvanic cell or an optional zirconium oxide sensor for  $O_2$  measurements. The standard detection ranges for  $CO_2$ ,  $SO_2$  and  $SO_2$  and  $SO_2$  and  $SO_3$  are  $SO_2$  and  $SO_3$  are  $SO_3$  on  $SO_3$  and  $SO_3$  are  $SO_3$  on  $SO_3$  and  $SO_3$  on  $SO_3$  on  $SO_3$  and  $SO_3$  on  $SO_3$  on SO

Because the concentrations of  $CO_2$  and other pollutants emitted from  $O_2/CO_2$  and  $O_2/RFG$  coal combustion system are much higher than the detection limits of flue gas analyzer, the dilution of flue gas is required before analysis. For minimizing the analysis errors resulted from gas dilution, highly precise gas dilution system was used and the dilution ratio was controlled as low as possible.

#### 3. Results and discussions

### 3.1. Emission characteristics of $O_2/RFG$ coal combustion with different feed gas compositions

Fig. 2 shows the variations of  $CO_2$ ,  $SO_2$  and NOx in the flue gas of coal combustion with different feed gas compositions (without recycling flue gas). At the same  $O_2$  concentration in the feed gas, the concentration of  $CO_2$  emitted from  $O_2/CO_2$  coal combustion is obviously higher than that from  $O_2/N_2$  combustion. Especially for the feed gas composition of  $21\% \ O_2/79\% \ N_2$ , which is same with general air, only  $13\% \ CO_2$  is produced in the coal combustion, while near  $98\% \ CO_2$  is produced in the  $O_2/CO_2$  coal combustion at the same feed gas concentration. Moreover, the concentrations of  $CO_2$  produced from  $O_2/N_2$  coal combustion are increased with the concentration of  $O_2$  in the feed gas. The highest  $CO_2$  concentration produced from  $O_2/N_2$  coal combustion is 34% at the feed gas composition  $50\% \ O_2/50\% \ N_2$ . The concentration of  $SO_2$  generated from  $O_2/N_2$  combustion is higher than  $O_2/CO_2$  combustion, and is increased with the  $O_2$ 

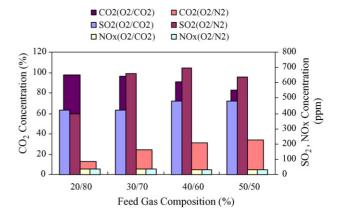


Fig. 2. Concentrations of CO<sub>2</sub>, SO<sub>2</sub> and NOx at different feed gas compositions (without recycled flue gas).

concentration in feed gas. The formation of NOx do not have significant variation in  $O_2/CO_2$  or  $O_2/N_2$  combustion. From the viewpoint of  $CO_2$  separation and recovery in a combustion process,  $O_2/CO_2$  is better than  $O_2/N_2$  because high-concentration  $CO_2$  is emitted as the carry gas is  $CO_2$  rather than  $N_2$ . Moreover, the specific heat of  $CO_2$  is higher than  $N_2$  and thermal stability of coal combustion in  $O_2/CO_2$  is higher than that in  $O_2/N_2$ .

### 3.2. Emission characteristics of $O_2/RFG$ coal combustion with different feed gas concentrations

Figs. 3 and 4 show the concentrations of  $CO_2$ ,  $SO_2$  and NOx in the flue gas of coal combustion at different feed gas concentrations of  $O_2/CO_2$  as the ratio of recycled flue gas are 40% and 50%, respectively. The maximum concentration of  $CO_2$  is higher than 95% at 30%  $O_2/70\%$   $CO_2$  feed gas and 40% or 50% recycled flue gas, the next is occurred at 40%  $O_2/60\%$   $CO_2$ . The formation of  $SO_2$  is similar to  $CO_2$ . The higher concentration is occurred at 30%  $O_2/70\%$   $CO_2$  or 40%  $O_2/60\%$   $CO_2$ . However, the formation of NOx is quite different from that of  $CO_2$  and  $SO_2$ , and more NOx are formed at the feed gas concentrations of 20%  $O_2/80\%$   $CO_2$  and 50%  $O_2/50\%$   $CO_2$ .

Figs. 5 and 6 show the concentrations of  $CO_2$ ,  $SO_2$  and NOx in the flue gas of coal combustion at different feed gas concentrations of  $O_2/N_2$  as the ratio of recycled flue gas are 40% and 50%,

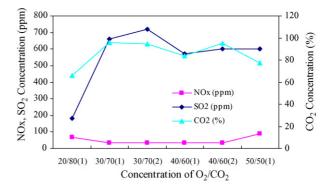


Fig. 3. Concentrations of CO<sub>2</sub>, SO<sub>2</sub> and NOx at different feed gas concentrations of O<sub>2</sub>/CO<sub>2</sub> with 40% recycled flue gas.

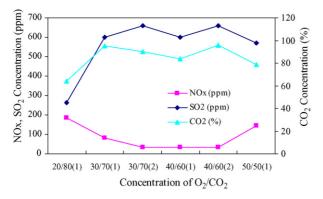


Fig. 4. Concentrations of  $CO_2$ ,  $SO_2$  and NOx at different feed gas concentrations of  $O_2/CO_2$  with 50% recycled flue gas.

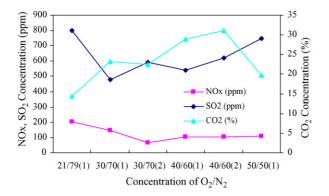


Fig. 5. Concentrations of  $CO_2$ ,  $SO_2$  and NOx at different feed gas concentrations of  $O_2/N_2$  with 40% recycled flue gas.

respectively. The maximum concentration of  $CO_2$  is occurred at 40%  $O_2/60\%$   $N_2$  with 40% or 50% recycled flue gas. The formations of  $SO_2$  and NOx are both higher at 21%  $O_2/79\%$   $N_2$  or 50%  $O_2/50\%$   $N_2$ . These results also demonstrate that the formation of NOx is significant in general air and oxygen-rich combustions. With 30% and 60% recycled flue gas, the maximum concentration of  $CO_2$  is occurred at 50%  $O_2/50\%$   $N_2$ . Comparing the results of coal combustion with  $O_2/CO_2$  and  $O_2/N_2$  feed gas atmosphere (Figs. 3–6), the concentration of  $O_2$  in the feed gas has different effects on the combustion characteristics and the formations of  $CO_2$ ,  $SO_2$  and NOx.

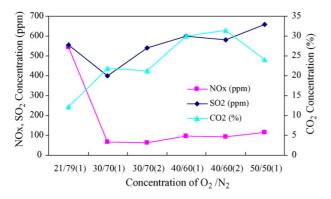


Fig. 6. Concentrations of  $CO_2$ ,  $SO_2$  and NOx at different feed gas concentrations of  $O_2/N_2$  with 50% recycled flue gas.

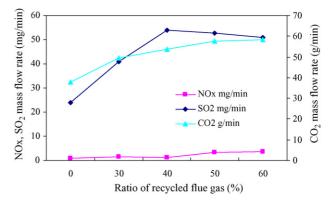


Fig. 7. Mass flow rate of  $CO_2$ ,  $SO_2$  and NOx at 30%  $O_2/70\%$   $CO_2$  feed gas with different recycled flue gas ratios.

### 3.3. Emission characteristics of $O_2/RFG$ coal combustion with different injection sites of recycled flue gas

For studying the effects of different injection sites of recycled flue gas on the performance of coal combustion, the recycled flue gas is injected into first combustion chamber and second combustion chamber, respectively (as shown in Fig. 1). The number in the parentheses of graduations on the horizontal axis of Figs. 3-6 indicates the injection site of recycled flue gas. From the results of Figs. 3-6, the concentration of CO<sub>2</sub> produced in the case of injecting recycled flue gas into the second combustion chamber is lower than that into first combustion chamber at the same ratio of flue gas recycled and the same feed gas composition of 30%/70% O<sub>2</sub>/N<sub>2</sub> or O<sub>2</sub>/CO<sub>2</sub>. However, the concentration of CO<sub>2</sub> produced from injecting recycled flue gas into the second combustion chamber becomes higher than that into first combustion chamber as the feed gas concentration gas is 40%/60%. This phenomenon is attributed to the different reaction intensities, combustion temperatures and retention time in these two combustion chambers as the flue gas is recycled into the first and second combustion chambers.

### 3.4. Emission characteristics of $O_2/RFG$ coal combustion with different ratios of recycled flue gas

With different ratios of recycled flue gas, the mass flow rates of  $CO_2$ ,  $SO_2$  and NOx in the flue gas are shown in Figs. 7–10. The mass flow rates of  $CO_2$  are increased with the ratios of recycled flue gas except for the feed gas composition  $20\%\ O_2/80\%\ CO_2$ . Recycling flue gas, which also recycles the pollutants, may enhance the concentrations of pollutants in the exhausted gas. This increased concentration is beneficial for the control, separation and recovery of  $CO_2$  and other pollutants. The mass flow rates of  $SO_2$  and NOx in the flue gas also have similar trends, only some exceptions are observed at the feed gas composition  $O_2/N_2$ . Above results indicate that coal combustion with recycled flue gas not only recovers the heat in the flue gas but also increases the mass flow rate of air pollutants because the volume of  $N_2$  in feed gas is reduced and the combustion efficiency is improved due to the increase of average retention time of

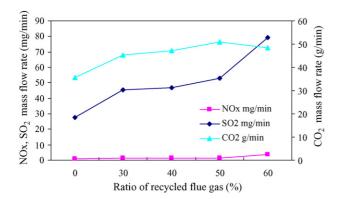


Fig. 8. Mass flow rate of  $CO_2$ ,  $SO_2$  and NOx at  $40\% O_2/60\% CO_2$  feed gas with different recycled flue gas ratios.

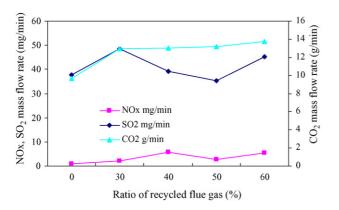


Fig. 9. Mass flow rate of  $CO_2$ ,  $SO_2$  and NOx at 30%  $O_2/70\%$   $N_2$  feed gas with different recycled flue gas ratios.

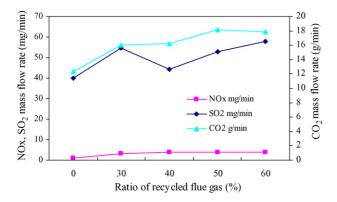


Fig. 10. Mass flow rate of  $CO_2$ ,  $SO_2$  and NOx at 40%  $O_2/60\%$   $N_2$  feed gas with different recycled flue gas ratios.

reactants in combustion system. With suitable gas composition  $O_2/CO_2$  and sufficient  $O_2$  concentration in the feed gas, higher combustion efficiency and effective control of air pollutants during coal combustion can be achieved.

### 4. Conclusions

This study investigates the emission characteristics of CO<sub>2</sub>, SO<sub>2</sub>, NOx in the flue gas of O<sub>2</sub>/RFG coal combustion with different feed gas compositions (O<sub>2</sub>/CO<sub>2</sub>/N<sub>2</sub>) and ratios of recycled flue gas. The concentration of CO<sub>2</sub> generated from O<sub>2</sub>/CO<sub>2</sub>

combustion is much higher than that from  $O_2/N_2$  combustion; the average concentration of  $CO_2$  is higher than 90% and is beneficial to separate  $CO_2$  from the flue gas by absorption or adsorption. The concentration of  $CO_2$  generated from  $O_2/N_2$  combustion is increased with the  $O_2$  concentration in feed gas and the maximum concentration of  $CO_2$  is near 34%.

In O<sub>2</sub>/CO<sub>2</sub> (O<sub>2</sub>/RFG) combustion, the maximum concentrations of CO<sub>2</sub> and SO<sub>2</sub> are both generated at the feed gas 30%  $O_2/70\%$   $CO_2$ , and the next is at 40%  $O_2/60\%$   $CO_2$ . The higher concentration of NOx is generated at 20% O<sub>2</sub>/80% CO<sub>2</sub> or 50% O<sub>2</sub>/50% CO<sub>2</sub>. Except for the feed gas 20% O<sub>2</sub>/80% CO<sub>2</sub>, the mass flow rates of CO2, SO2, and NOx in the flue gas are all increased with the ratio of recycled flue gas. This result indicates that O<sub>2</sub>/RFG combustion technology is really effective in enhancing the mass flow rates of CO<sub>2</sub> and other pollutants. The treatment efficiency of air pollution control devices or the separation and recovery efficiency of CO<sub>2</sub> can be therefore improved. In  $O_2/N_2$  combustion, the maximum concentration of  $CO_2$  is generated at 50% O<sub>2</sub>/50% N<sub>2</sub>, while the maximum concentration of SO<sub>2</sub> and NOx is generated at 21% O<sub>2</sub>/79% N<sub>2</sub> or 50% O<sub>2</sub>/50% N<sub>2</sub>. The formation of NOx in conventional air combustion or oxygen-rich combustion is significant. Increasing the ratios of recycled flue gas, the mass flow rate of CO<sub>2</sub> in the flue gas is slightly increased and that of SO<sub>2</sub> and NOx are unapparent.

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